

CONSTRUISSONS **ENSEMBLE**  
LA DÉFENSE DE DEMAIN

# CONSIDERATIONS ON THE WAY TO DUPLICATE THE NATO STANDARD LIQUID FUEL FIRE FOR THE FCO TEST

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# Abstract reference n°17237



# Summary

- **Background : from Meppen to Rome...**
- **What is the Standard kerosene pool fire ?**
- **What are the Alternative fuel fires ?**
- **Numerical Approach : Simulations of the standard and alternative fuel fires**
  - Computed thermal environment around the munitions
  - Effect of munitions emissivity on radiative transfer and munitions surface temperature
  - Effect of setup parameters on thermal environment around the munitions
- **Discussion / Conclusion**



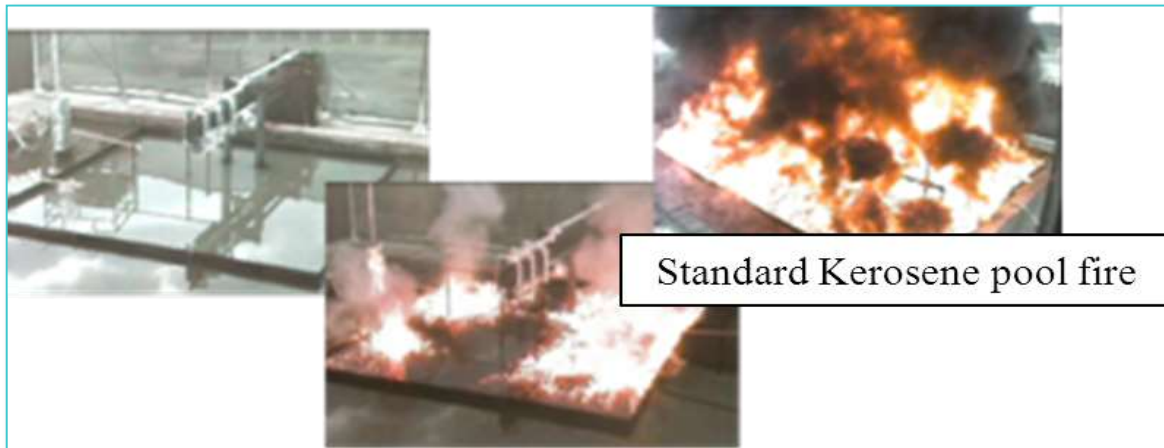
# Background

## Fast Cook Off Test :

- NATO standard IM test to evaluate the reaction level of the munitions when engulfed in a liquid kerosene fuel fire
- One of the UN standard tests to determine the hazard classification of the munitions

## How to mimic the Standard Kerosene Pool Fire ?

- NATO Fuel Fire Experts Meetings from 2010 to 2015
- Discussion about the introduction of an alternative way to do fast heating



Background

Liquid Fuel  
Fire

Alternate  
Fuel Fire

Modeling

Results

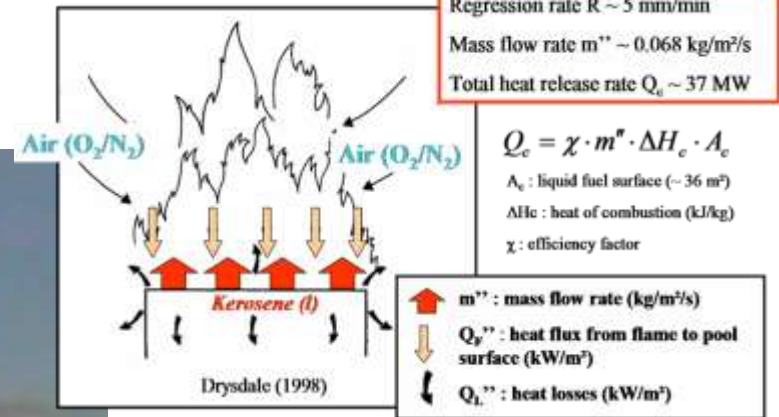
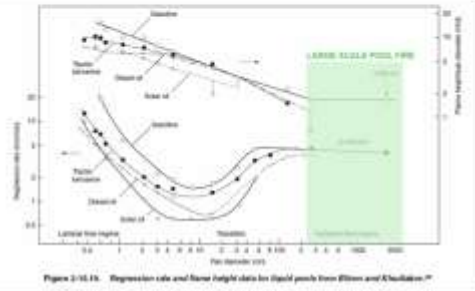
Conclusion



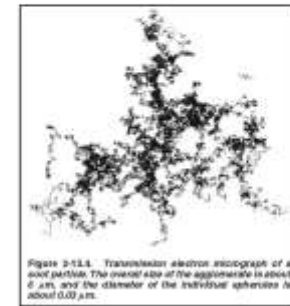
# What is the Standard Kerosene Pool Fire ?

## Large-scale pool fire

- Pool diameter ~ 4-6 meters
- L/d ~ 2-2.5
- Turbulent flow regime



Flame temperature ~ 800-1100°C  
 Gas (CO<sub>2</sub>, H<sub>2</sub>O, CO, ...) + Particles (Soot)  
**Very sooty flame plume**



Mulholland (1998)

But convective heat transfer not predominant

Heat Transfer to the surroundings and into the flames is mainly due to RADIATION from :

- Luminous flame
- Hot gases (CO<sub>2</sub>, H<sub>2</sub>O, CO)
- Soot particles (Rayleigh diffusion)

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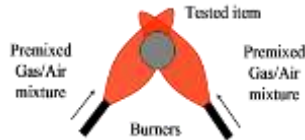


# What are the Alternative Fuel Fires ?

## Swedish/Dutch-type setup : premix Gas/Air injection



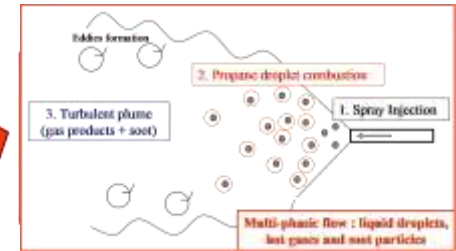
Toreheim et al. (2010)



Scholtes et al. (2013)

## German-type setup : Liquified Propane Gas Injection

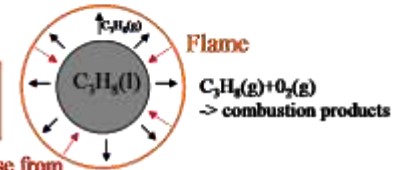
Weigand et al. (2010)



German setup (WTD91, Meppen)

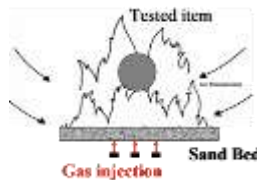
Fuel Droplet combustion

Combustion law (diffusion flame) :  
 $d^2(t) = d_0^2 - k \cdot t$  with  $k(\rho_p, B_{sp,0}, Sh, D_p)$



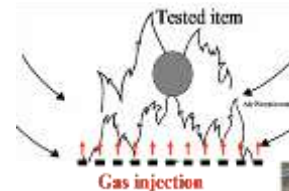
Heat release from flame to droplet

## New Swedish-type setup : LPG injection within a sand bed



Toreheim et al. (2013)

## US-type setup : Propane gas injection



Hubble et al. (2014)

Background

Liquid Fuel Fire

Alternate Fuel Fire

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# Standard Kerosene Pool fire vs Alternative Fuel Fires

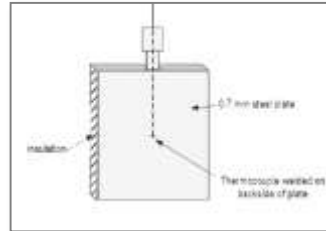
| Test facility          | Standard Kerosene Pool                      | German-type                                  | Dutch-type                                      | New Swedish-type                             | US-type                                  |
|------------------------|---|--|---|--|--|
| <b>Fire</b>            | Pool fire                                   | LPG droplet spray                            | Premixed Gas/Air Mixture                        | LPG within a sand bed                        | LPG                                      |
| <b>Combustion</b>      | Liquid fuel combustion                      | Propane liquid droplet combustion            | Premixed Gas/Air flame combustion               | Liquid fuel combustion                       | Liquid fuel combustion                   |
| <b>Flow regime</b>     | Turbulent (vertical)                        | Turbulent (horizontal jet)                   | Laminar or turbulent (mass flow rate dependent) | Turbulent (vertical)                         | Turbulent (vertical)                     |
| <b>Burnt gases</b>     | CO <sub>2</sub> ,CO,H <sub>2</sub> O,...    | CO <sub>2</sub> ,CO,H <sub>2</sub> O, ...    | CO <sub>2</sub> ,CO,H <sub>2</sub> O,...        | CO <sub>2</sub> ,CO,H <sub>2</sub> O, ...    | CO <sub>2</sub> ,CO,H <sub>2</sub> O,... |
| <b>Soot production</b> | Black smoky plume<br>Unobservable munitions | Yellow/orange flame<br>Munitions can be seen | Blue/orange flame<br>Munitions can be seen      | Yellow/orange flame<br>Munitions can be seen | Orange flame<br>Munitions can be seen    |

# What about the thermal load ?

- Fuel Fire Experts Meetings : from Meppen to Rome, a significant work to EXPERIMENTALLY characterize the thermal load induced by :
  - The Standard Kerosene pool fire
  - The Alternative Fuel Fires (German, Dutch, Swedish and American – types)
- Heat flux and temperature measurements within the standard and alternative fires by the US basket and other methods



*Yagla et al. (2013)*



*Wickstrom et al. (2012)*



*Chassagne et al. (2013)*

But few NUMERICAL investigations

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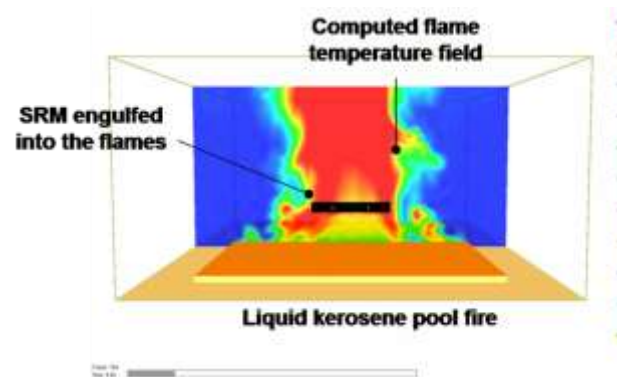
# French Numerical Approach

## OBJECTIVES :

- To assess the thermal load of the standard and alternative fires
- To compute the effect :
  - of munitions emissivity on radiative transfer and munitions surface temperature
  - of adjustable setup parameters on thermal load around the munitions

## MEANS :

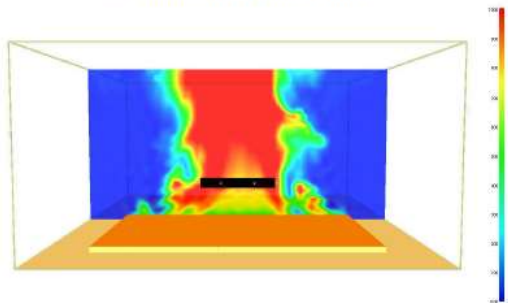
- CFD Code : Fire Dynamics Simulator v5 – developed by the NIST (USA) – typically used for fire safety issues (Mc Grattan et al. 2009)
- Low Mach number flows – Large Eddy Simulation (LES) – Mixture Fraction model
- Used to simulate large scale liquid fuel fires (FCO Test)



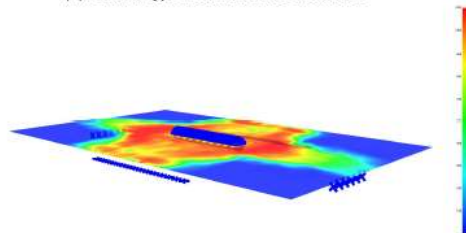


# Simulation of the thermal load around the munitions

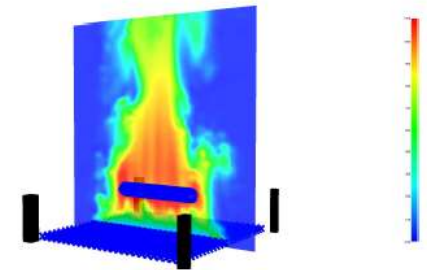
(a) Standard Liquid Fuel Fire Simulation



(b) German-type Alternative FireSimulation



(c) US-type Alternative FireSimulation



Thermal loads globally in the same order

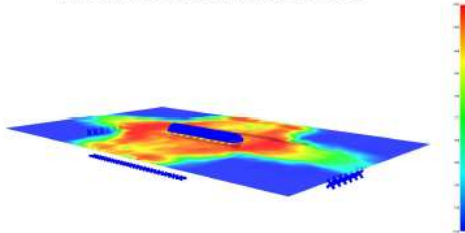
| Time-Averaged Values       |                                  | Standard Liquid Kerosene Fire | German-type Alternative Fire | US-type Alternative Fire |
|----------------------------|----------------------------------|-------------------------------|------------------------------|--------------------------|
| Flame Temperature (°C)     | $T_{upper}$                      | 831                           | 915                          | 882                      |
|                            | $T_{mid}$                        | 843                           | 881                          | 913                      |
|                            | $T_{et1}$                        | 822                           | 887                          | 804                      |
|                            | $T_{et2}$                        | 844                           | 877                          | 872                      |
|                            | $T_{base}$                       | 947                           | 817                          | 850                      |
|                            | $T_{en}$                         | 937                           | 823                          | 749                      |
| Incident Heat Flux (kW/m²) | $\Phi_{max}$                     | 128                           | 104                          | 115                      |
| Soot Production            | Integral of Soot Volume Fraction | 3.77 e-6                      | 8.49 e-7                     | 5.9 e-7                  |

Soot volume fraction has strongly decreased within the alternative fires

LPG Time-averaged Temperature > 800°C but... ..is it still realistic to assume  $\epsilon_{munitions} = 0.9$  during the whole test ?

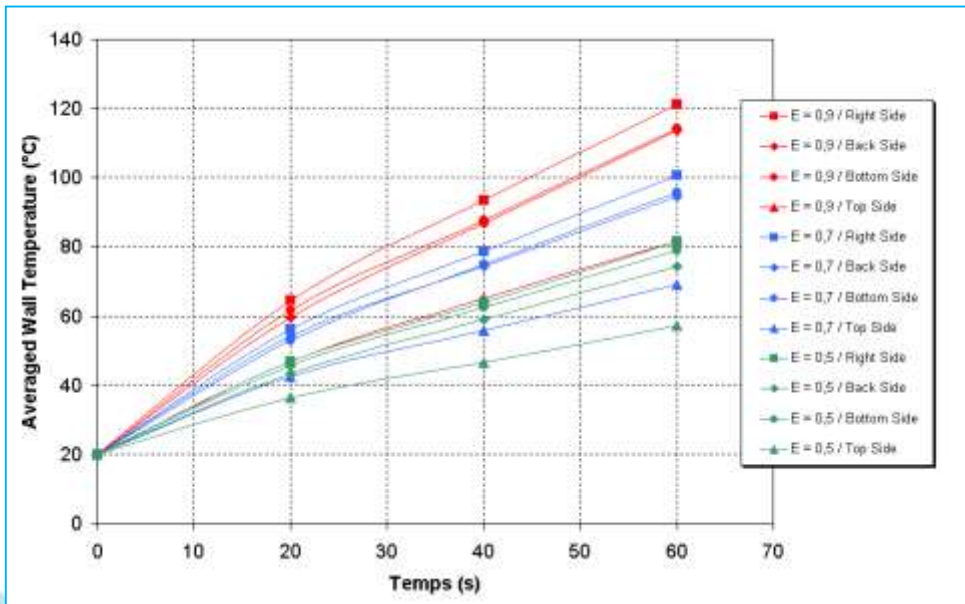
# Effect of munitions emissivity

(b) German-type Alternative FireSimulation



Droplet Flow Rate = 30 L/min – Nozzle-munition distance = 2.5 m – Munitions length : 2m

Lower soot production within alternative fires  
 $\epsilon_{munitions}$  may be not close to 1  
 Numerical simulations : German-type setup with  
 $\epsilon_{munitions} = 0.5$  to  $0.9$



To reduce  $\epsilon_{munitions}$  from 0.9 to 0.5



Munitions surface temperature

Reaction delay



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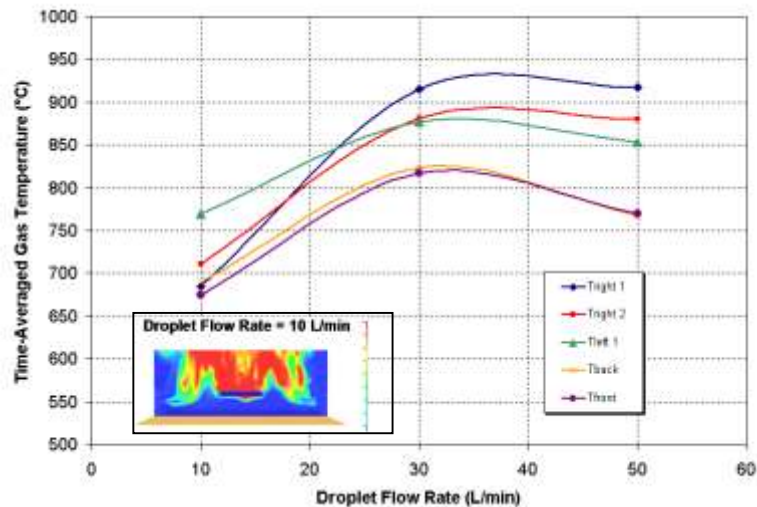


|            |                  |                     |          |         |            |
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| Background | Liquid Fuel Fire | Alternate Fuel Fire | Modeling | Results | Conclusion |
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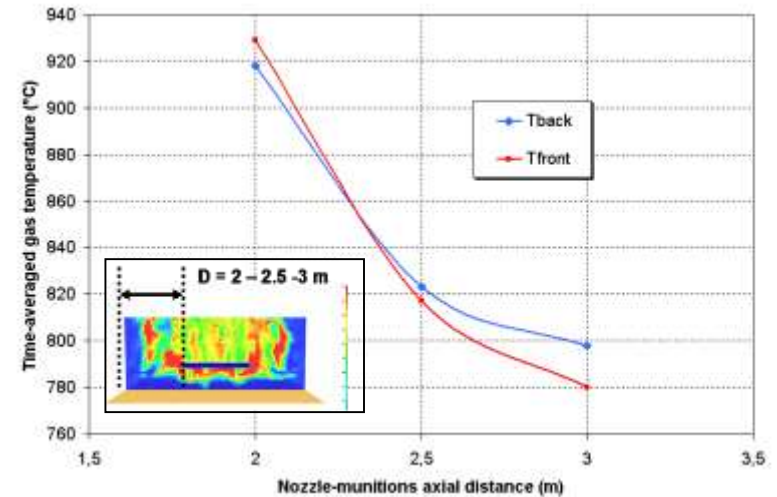


# Effect of LPG setup parameters

Droplet Flow Rate is reduced from 50 to 10 L/min



Nozzle-munitions distance = 2 – 2.5 – 3 meters



Gas temperature field (and so heat transfer) around the munitions strongly depends on the droplet flow rate and the nozzle-munitions distance

Experience and experimental tests are needed to determine the optimal value

Background

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# Discussion about numerical results

Numerical analysis showed that :

- 800°C gas temperature and 100 kW/m<sup>2</sup> heat flux can be achieved by Standard and Alternative fires but thermal load is not uniform along the munitions
- Standard Kerosene Fire produces pretty much soot particles
- To assume  $\epsilon_{\text{munitions}} = 0.9$  could be false in the Alternative cases because of a weaker soot production
- To assume  $\epsilon_{\text{munitions}} < 0.9$  may be more realistic but may induce weaker munitions surface temperature and higher reaction delay
- Thermal environment around the munitions depends on the LPG design and some adjustable key parameters (fuel flow rate, nozzle-munitions distance)



# Conclusion



Standard Kerosene pool fire



Alternative fuel fires



**Kerosene pool fire is still the Standard fire because :**

It is more linked with a real accidental scenario

It is not adjustable

It is well-adapted to the whole types of munitions (from large solid rocket motor to ammunition)

Strong feedback is still missing to assert equivalency in terms of reaction between Standard and Alternative fires

**Calibration of the Alternative fire test facilities is needed**

Calibration tests shall be in accordance with the tested munitions (dimension, time to reaction,...)

Both temperature and heat flux around the tested item shall be measured

Whatever the adjustments the alternative test facilities must be compliant with the future AOP 4240 requirements in terms of thermal load around the munitions

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**THANK YOU FOR YOUR ATTENTION**

**ANY QUESTIONS ?**