
Phase Diagram Modelling of Cast Energetic Materials

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IMEMTS 2015
21 May 2015



Outline

- Approach and Thermodynamic Basis
- Pure Components
 - TNT, RDX, HMX
- Binary Phase Diagrams
 - TNT – RDX & HMX – RDX Systems
- Summary



Approach

- Apply the principles of phase diagram modelling to systems involving energetic materials
- Determine what information is important in these systems



Thermodynamic Basis

- With the solid and the liquid of a pure compound in equilibrium:

$$\Delta G = \Delta H_m - T_m \Delta S_m = 0$$

$$\Delta S_m = \frac{\Delta H_m}{T_m}$$

- Once state variables fixed, the difference as a function of temperature is:

$$\Delta G_{s \rightarrow l} = \Delta H_m - T \Delta S_m$$



Thermodynamic Basis

- Problem: previous equation embodies differences
- Heat capacity, C_p , is measured directly
- Generalise for a specific phase: liq, α , ..

$$G = \Delta H_f^0 + \int_{T_{ref}}^T C_p dT - T \left(S_{ref}^0 + \int_{T_{ref}}^T \frac{C_p}{T} dT \right)$$

- Preserve differences in the ΔG
 - *Implicitly defined a reference phase*



Thermodynamic Basis - Binary Systems

- At constant temperature, equilibrium between two phases, α and β , occurs when the partial molar Gibbs energy of each of the two components A and B are equal in both phases:

$$\overline{G}_A^\alpha = \overline{G}_A^\beta \quad \text{and} \quad \overline{G}_B^\alpha = \overline{G}_B^\beta$$

- The Gibbs energy of a solution is described by:

$$\begin{aligned} G = & x_A G_A^{ref} + x_B G_B^{ref} + x_A G_A^{\Delta phase} + x_B G_B^{\Delta phase} \\ & + RT(x_A \ln x_A + x_B \ln x_B) \\ & + x_A x_B (p_0 + p_1 x_B + p_2 x_B^2 + \dots p_n x_B^n \dots) \end{aligned}$$



Computational Tools

- Partial molar Gibbs energy determined numerically
- Computations repetitive and onerous
- Use specific software written for the purpose:
 - Here, FactSage 6.4 and Fact 2.2



Pure Compound: TNT

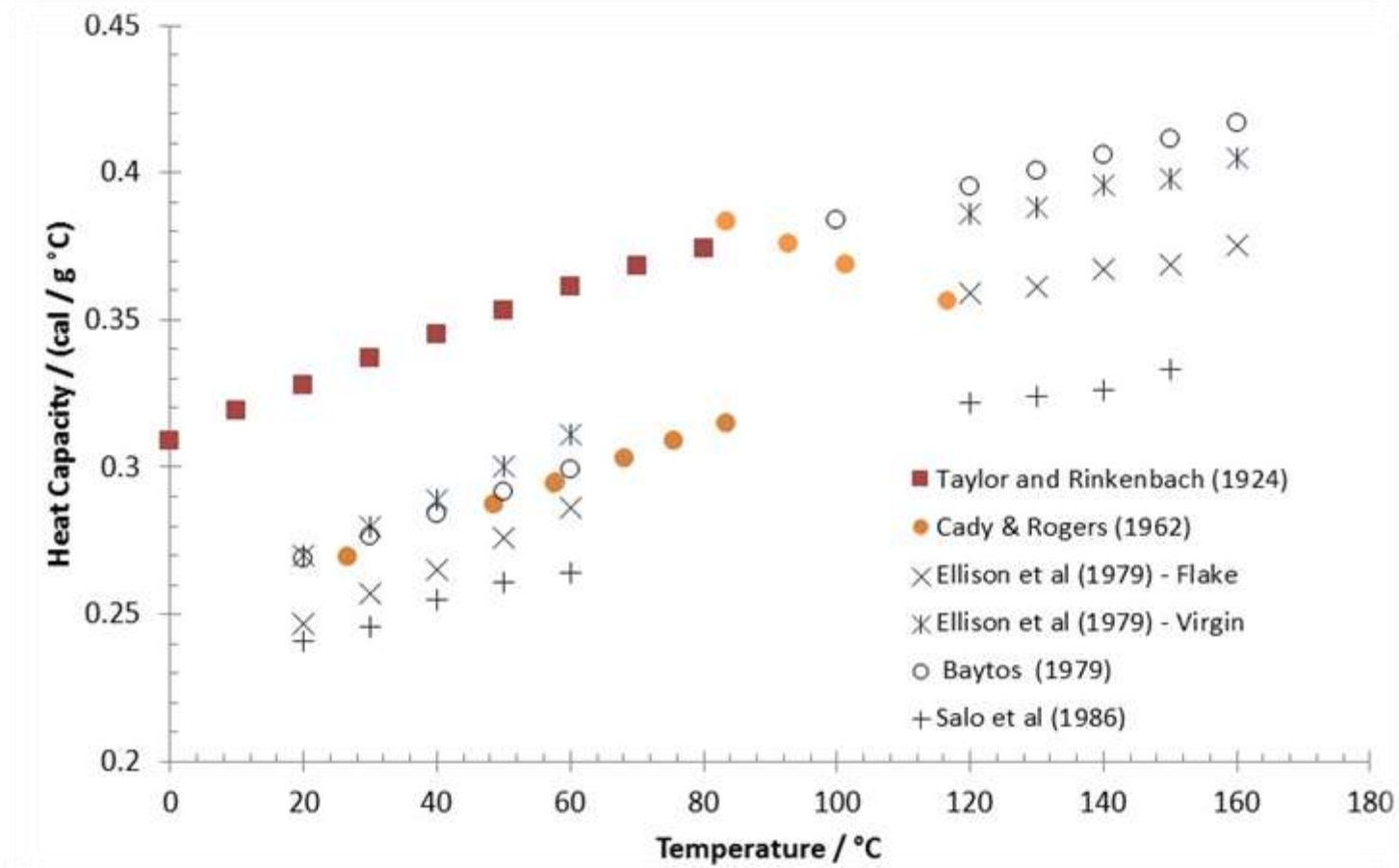
- $T_m = 80.8^\circ\text{C}$ (393.95 K)
- $\Delta_{\text{fus}} h^\circ = 23.5 \text{ cal g}^{-1}$ (5250 cal mol⁻¹)
- Heat capacity (cal mol⁻¹K⁻¹):

$$C_P^{\text{solid}} = 11.174 + 0.17035 T \text{ and}$$

$$C_P^{\text{liquid}} = 140.61 + 0.12488 T$$



Pure Compound: TNT



Heat capacity of TNT as a function of temperature.



Pure Compound: RDX

- $T_m = 205.3^\circ\text{C}$ (478.45 K)
- $\Delta_{\text{fus}} h^\circ = 7356 \text{ cal mol}^{-1}$
- Heat capacity:

$$C_P^{\text{solid}} = 7.489 + 0.15992 T \text{ and}$$

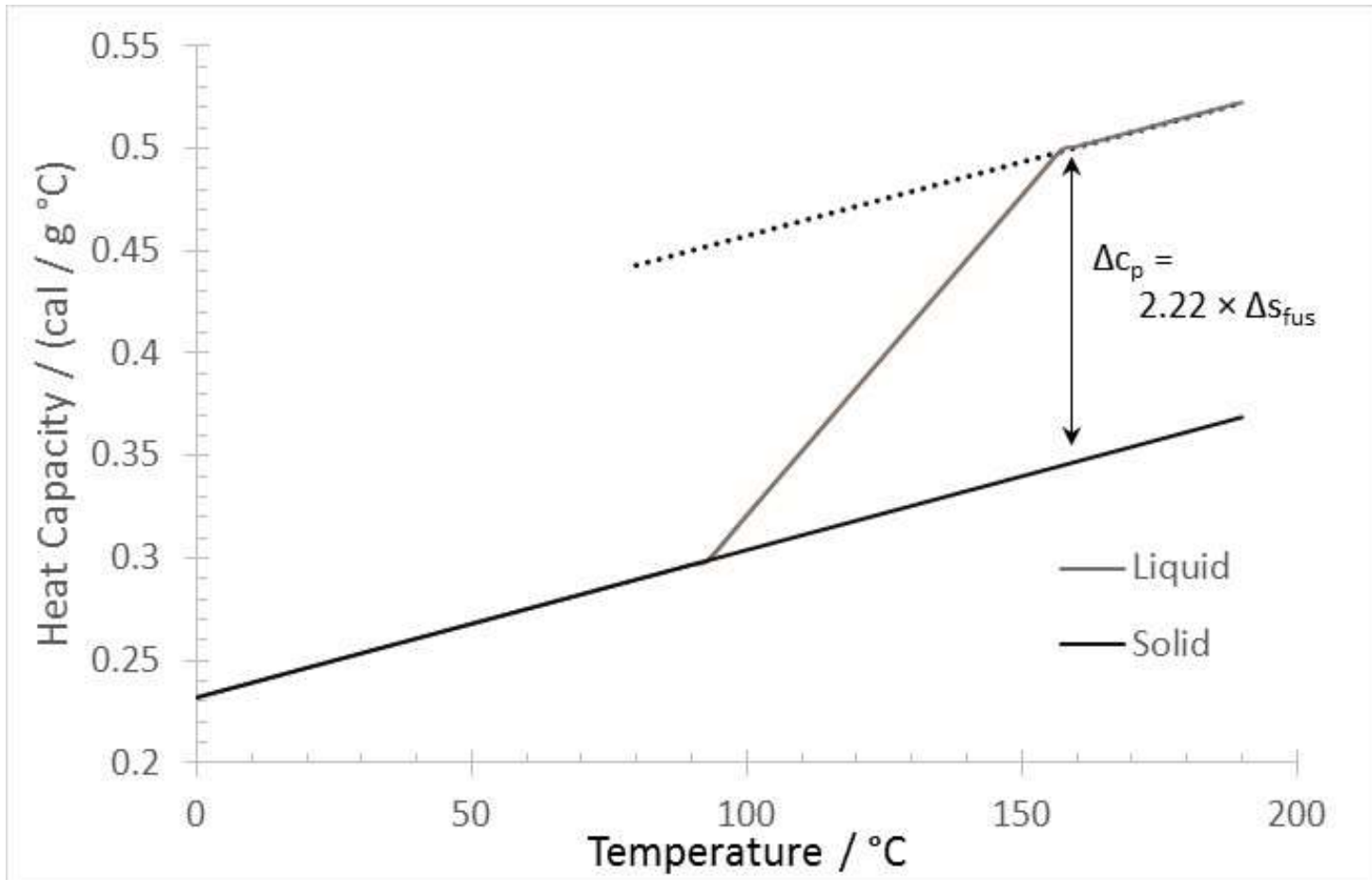
$$C_P^{\text{liquid}} = C_P^{\text{solid}}, \text{ for } T < 366 \text{ K}$$

$$C_P^{\text{liquid}} = -187.294 + 0.693 T, \text{ for } 366 \text{ K} < T < 430 \text{ K}$$

$$C_P^{\text{liquid}} = 42.011 + 0.15992 T, \text{ for } 430 \text{ K} < T$$



Pure Compound: RDX



Heat capacity of RDX solid and liquid as a function of temperature.



Pure Compound: HMX

- $T_m = 280.5^\circ\text{C}$ (553.65 K)
- $T_{\beta \rightarrow \delta} = 157^\circ\text{C}$ (430.15 K)
- $\Delta_{\text{fus}} h^\circ = 9036 \text{ cal mol}^{-1}$
- $\Delta h^\circ_{\beta \rightarrow \delta} = 2190 \text{ cal mol}^{-1}$
- Heat capacity:

$$C_P^{\text{solid}} = 23.916 + 0.1629T \text{ and}$$

$$C_P^{\text{liquid}} = C_P^{\text{solid}}, \text{ for } T < 415\text{K}$$

$$C_P^{\text{liquid}} = -157.419 + 0.600T, \text{ for } 415\text{K} < T < 498\text{K}$$

$$C_P^{\text{liquid}} = 60.181 + 0.1629T, \text{ for } 498\text{K} < T$$

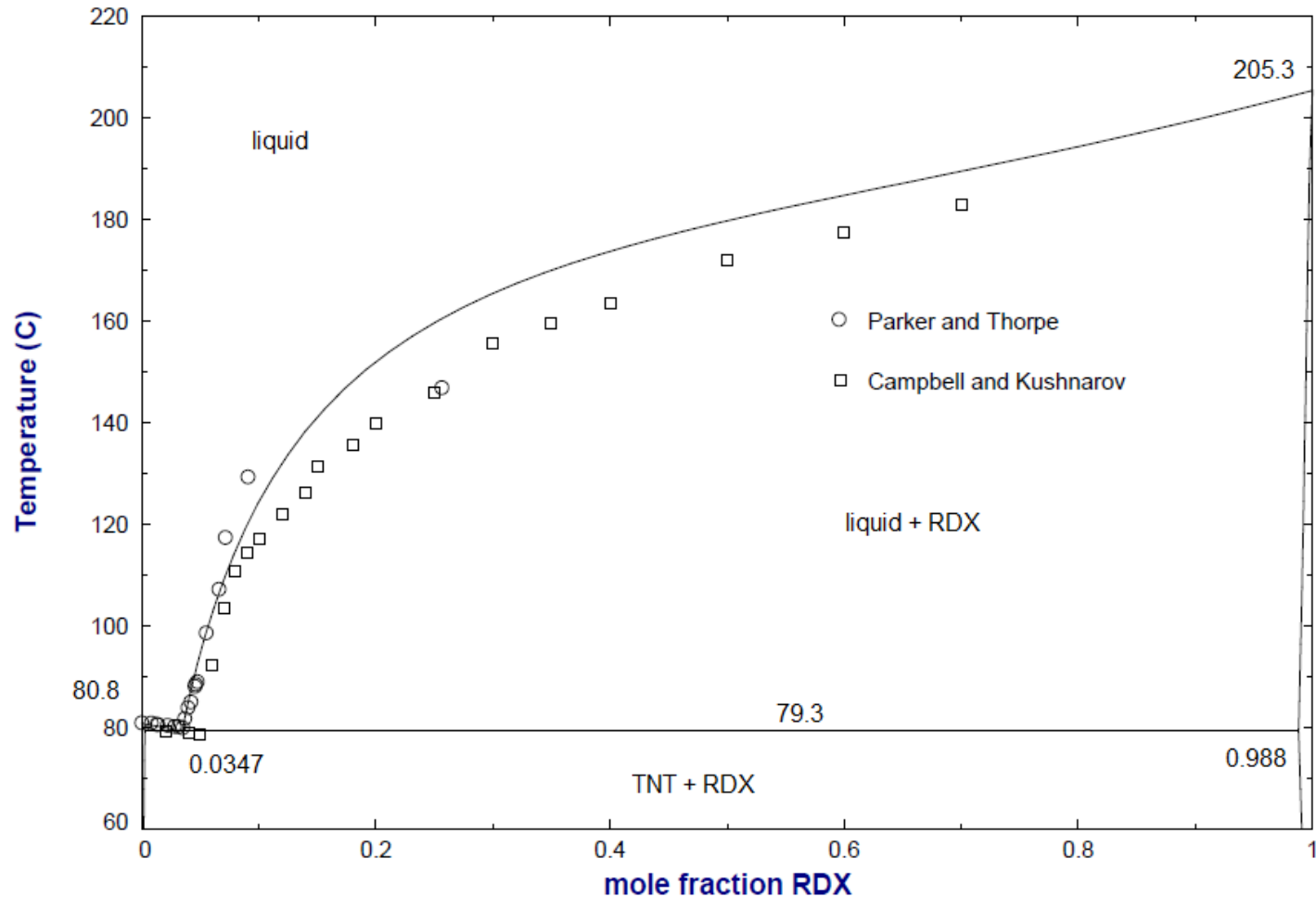


Binary Diagram: TNT – RDX

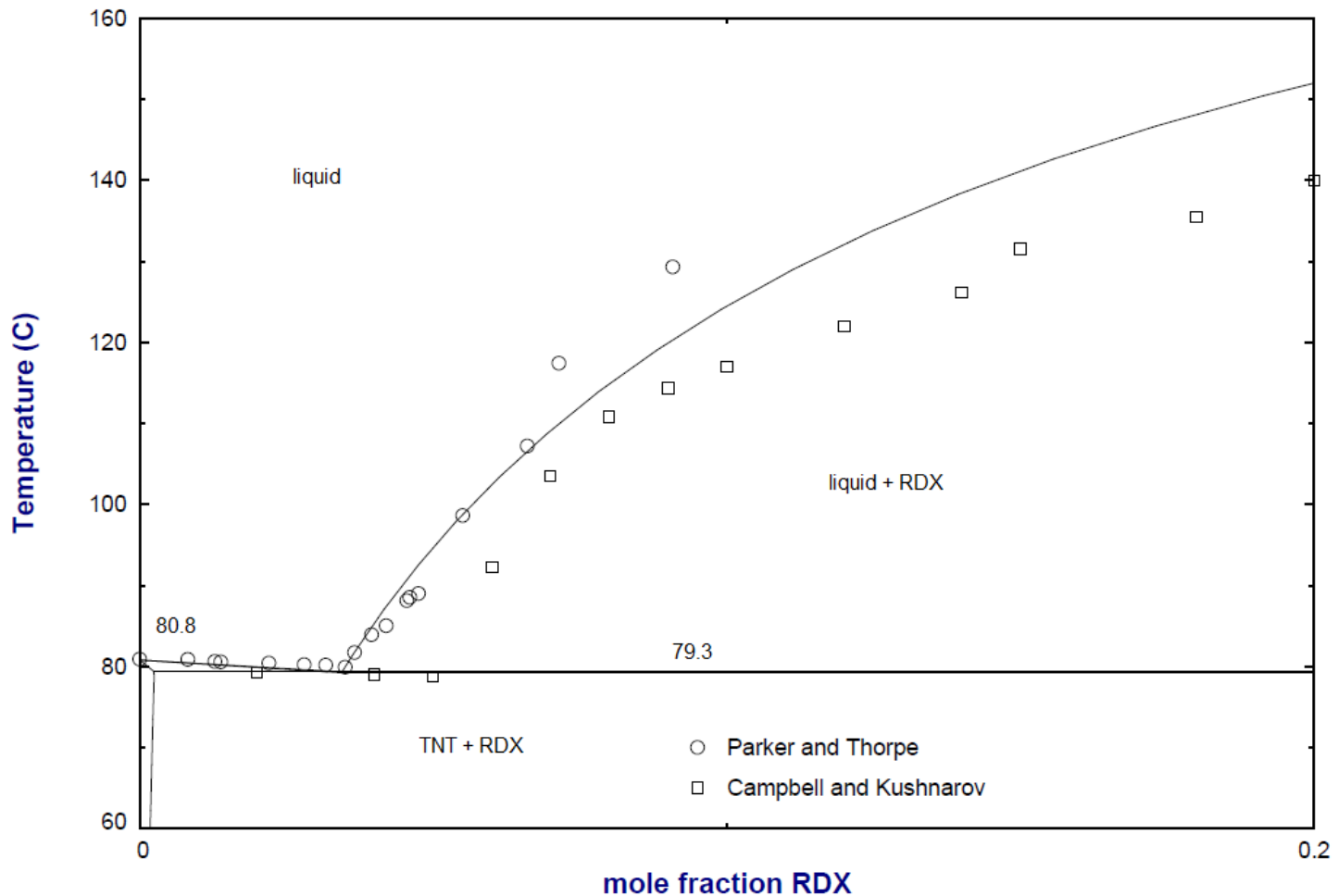
- RDX into TNT form: $+3100 \text{ cal mol}^{-1}$
- TNT into RDX form: $+3100 \text{ cal mol}^{-1}$
- Liquid: $G^{xs} = X_{\text{TNT}} X_{\text{RDX}} (1000 \text{ cal mol}^{-1})$



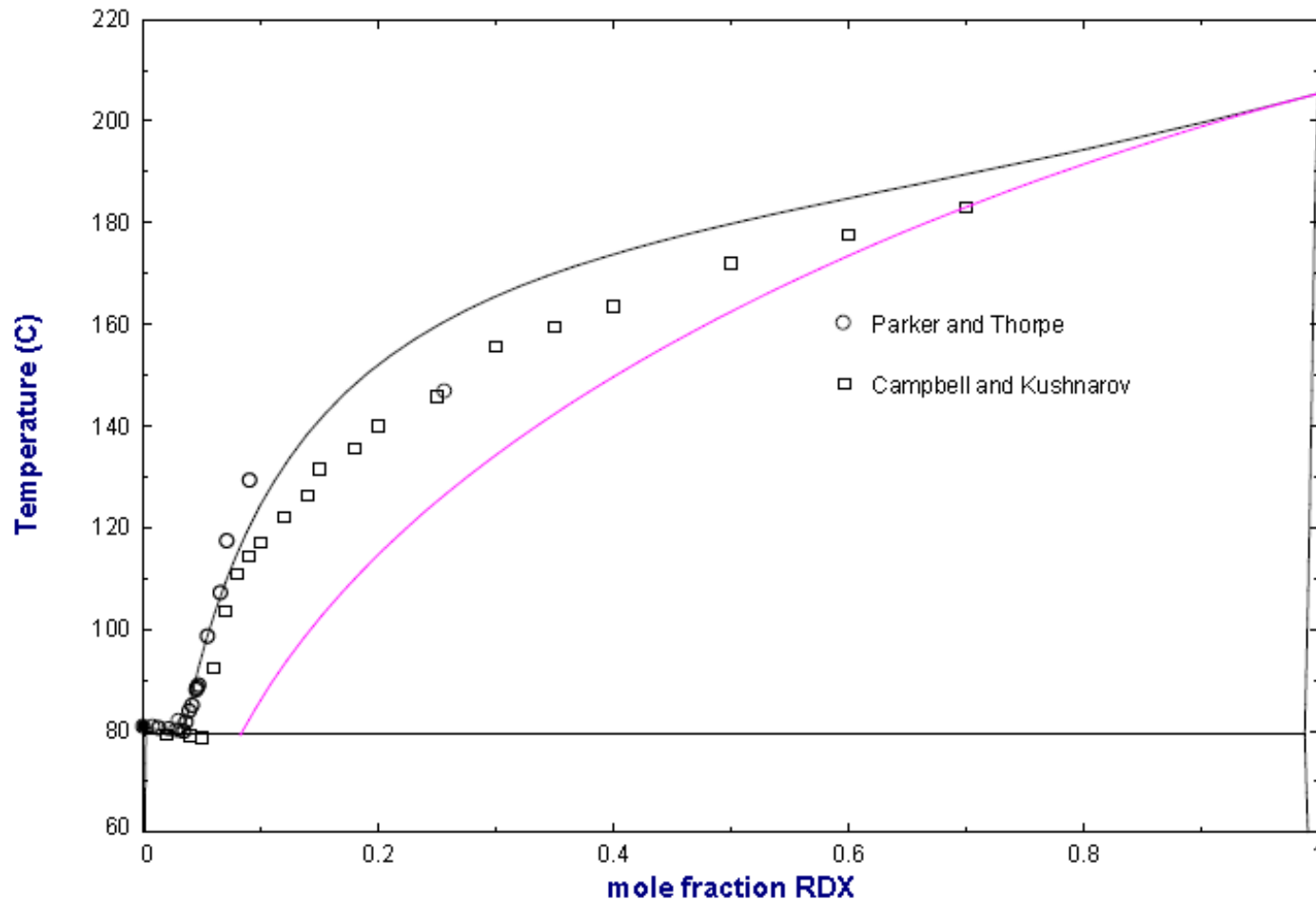
Binary Diagram: TNT – RDX



Binary Diagram: TNT – RDX



Binary Diagram: TNT – RDX



Change in Heat Capacity

- Magnitude of excess energy:
 - $G^{XS} = X_{TNT}X_{RDX}(1000 \text{ cal mol}^{-1})$
 $= 250 \text{ cal mol}^{-1}$ at $x=0.5$
- Magnitude of change in heat capacity:
 - $\Delta C_p \times \Delta T = (5 \text{ cal mol}^{-1} \text{K}^{-1}) \times 50 \text{ K}$
 $= 250 \text{ cal mol}^{-1}$
- Getting ΔC_p information important

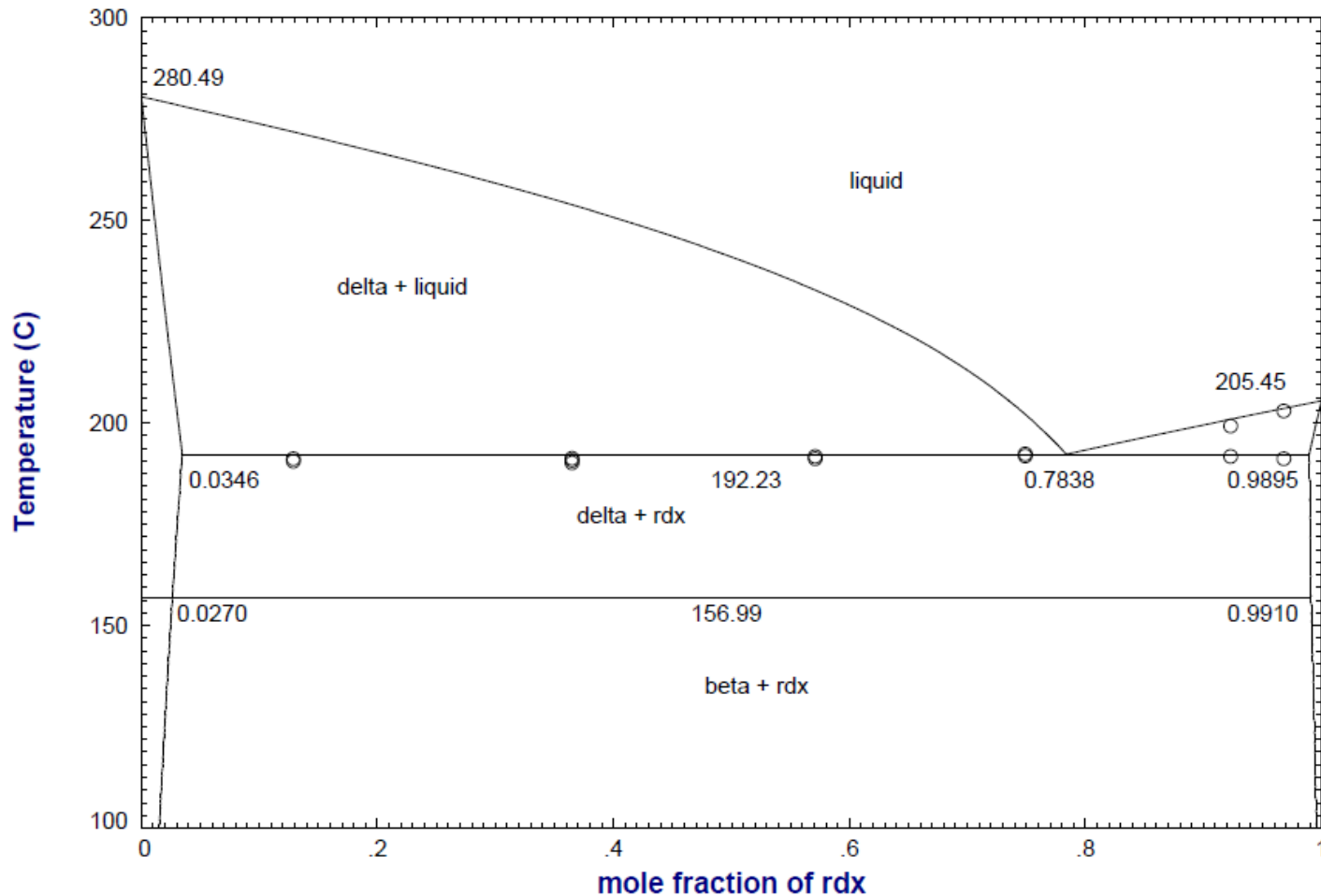


Binary Diagram: HMX – RDX

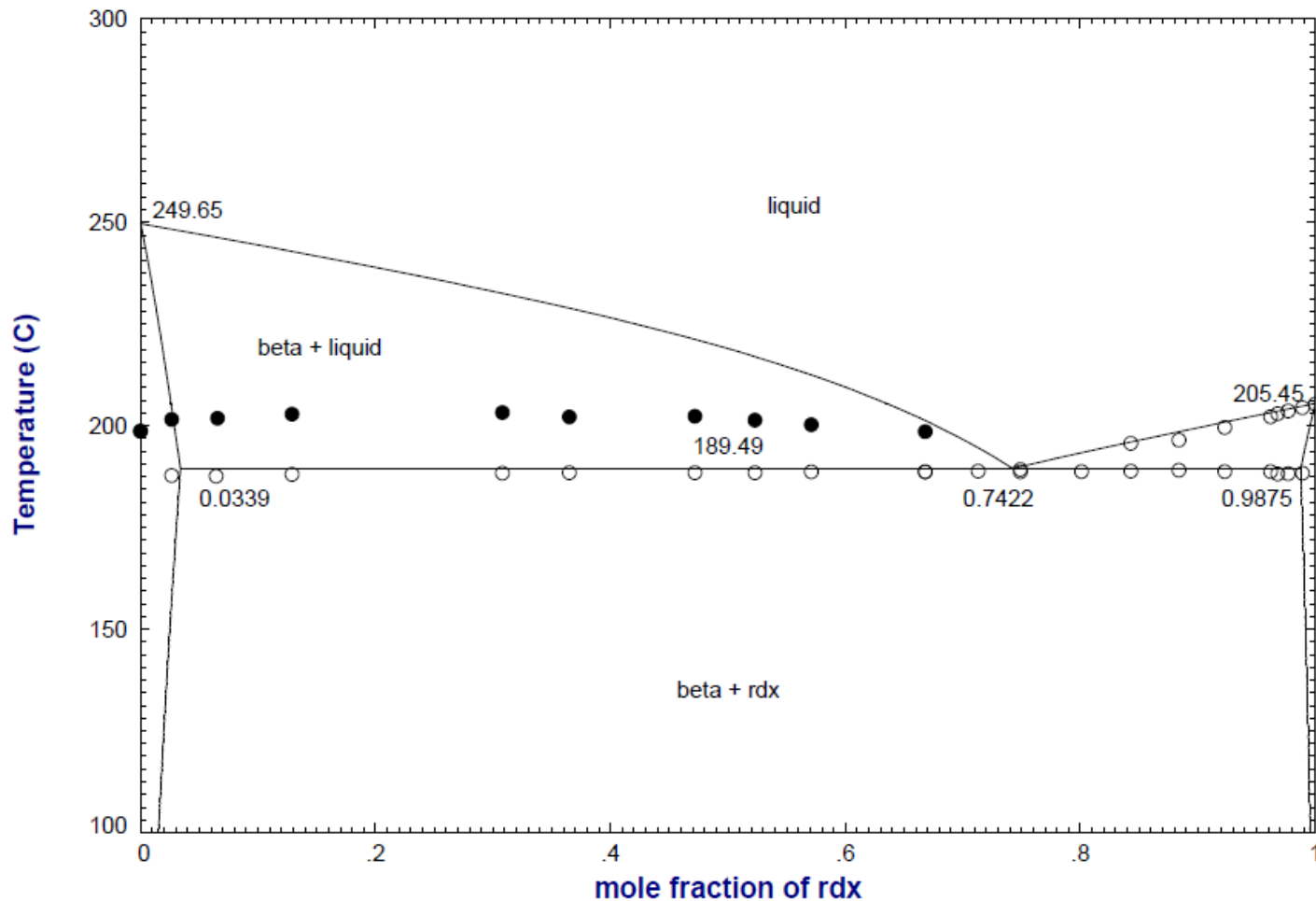
- RDX into HMX forms: +3100 cal mol⁻¹
- HMX into RDX form: +4000 cal mol⁻¹
- Liquid: $G^{xs} = X_{\text{HMX}}X_{\text{RDX}}(400 \text{ cal mol}^{-1})$



Binary Diagram: HMX – RDX



Binary Diagram: HMX – RDX



Energetics in HMX - RDX

- Energy expressions as a function of composition for the solutions
- Potential to investigate energy differences between phases
 - Nucleation Barrier
 - Mass Transfer



Summary

- Phase diagram features are
 - More dependent on the behavior of pure components
 - Less dependent on interactions in a (solid) solution
- Heat capacity is important
- Further work looking at better models and specific energetics of the transformation in HMX



Thank you for your attention

Questions?



