



# Modelling tool for industrial application – Melt-cast ammunitions

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# Summary

## Thales VTS Fr activities

## Need of numerical tool for cooling optimization phase

- Objectives
- Data acquisition

## Modelling interface

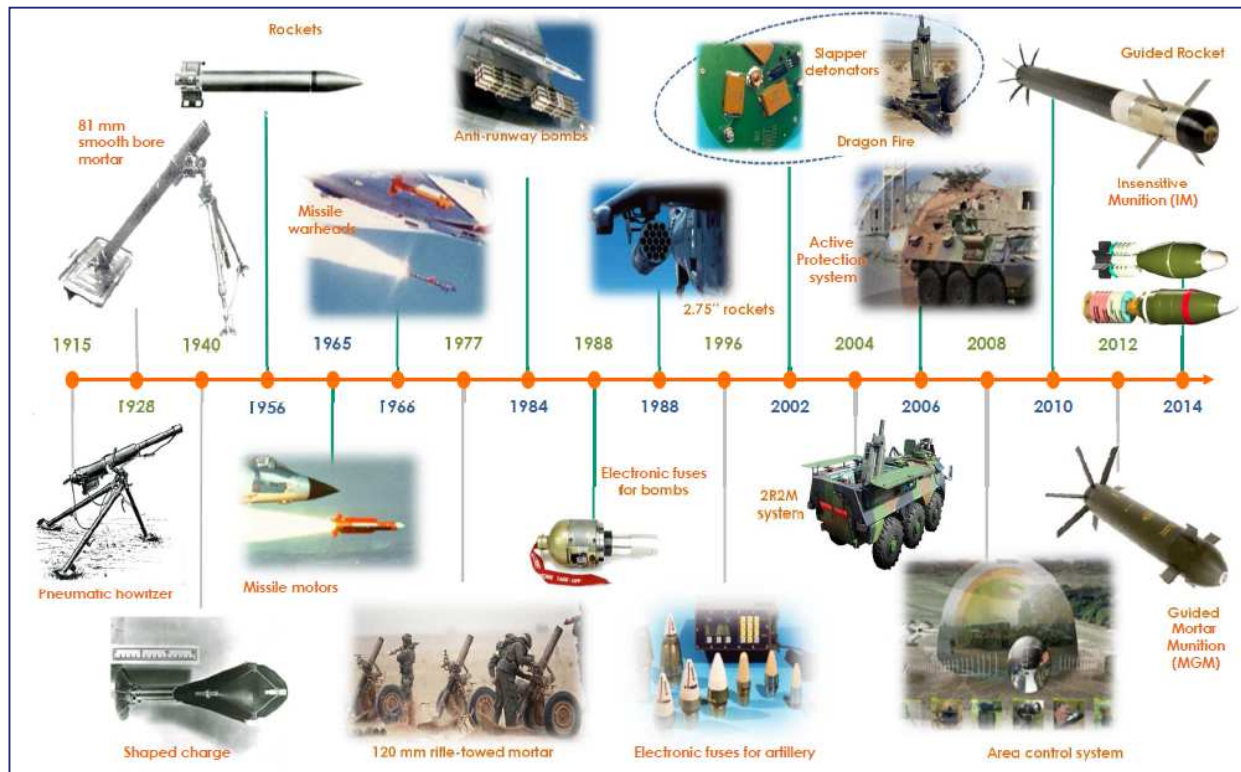
- Geometry parametrization
- Cooling process

## Experimental study on retract

## Conclusion

# Thales VTS Fr activities

## Last centuries



Mortar  
Shaped charge  
Rockets  
Anti-runway bomb  
Pyrotechnics components  
Area control system  
Active protection systems  
Guided rocket  
Guided mortar  
Inensitive Munitions

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# Need of a numerical tool for cooling optimization phase

## Objectives

Development of a numerical tool to implement TNT-based explosive composition in a shell body

- Whatever the shell
- Whatever the energetic material formulation
- Quick definition of set parameters for industrial equipment
- HMI for industrial use

# Need of a numerical tool for cooling optimization phase

## Data Acquisition on melt-cast process

### ➤ Process parameters

- Preheating phase
- Formulation process
- Controlled solidification

### ➤ Ammunition design

- 120/81 mm mortar ammunitions
- Shaped charge
- Rockets

### ➤ Energetic materials

- Liquid and solid density
- Thermal properties

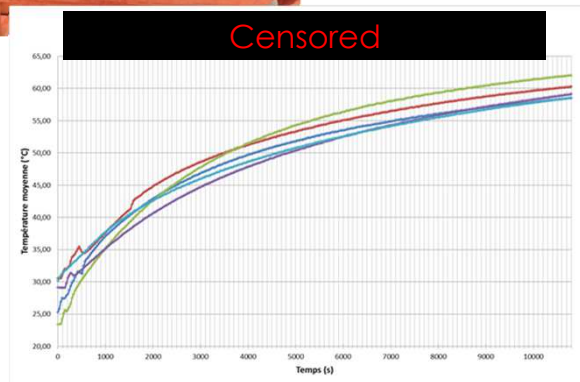
# Modelling interface

## Process parameters

### ➤ Preheating system analyses



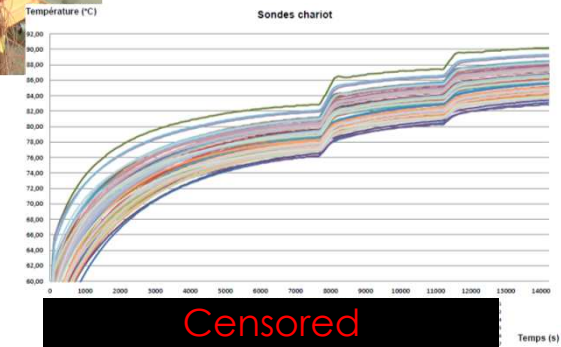
- 120 probes
- 2 temperatures
- 6 h registration
- 6 cart's positions
- 2 weeks studies



### ➤ Cooling system characterization



- 72 probes
- 3 temperatures
- 4 h registration
- 12 positions
- 1 week



Abacus

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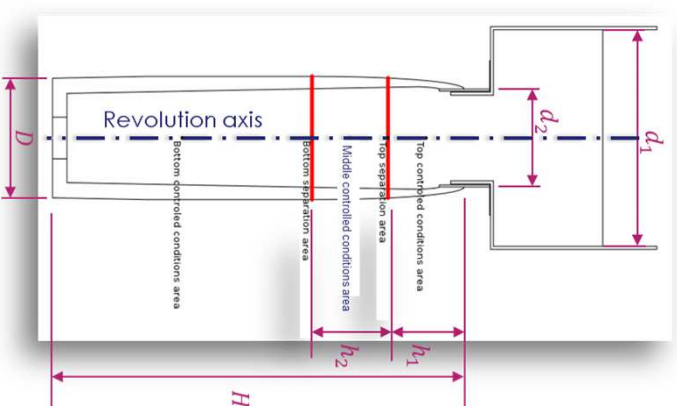
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# Modelling interface

## Geometry parametrization

### ➤ Fully parametrised

**Axisymmetric model**  
Heat equation solved:  
$$\rho C_p \frac{\partial T}{\partial t} - \nabla \cdot (k \nabla T) = 0$$



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**Boundary condition: heat flux**  
$$q = h \cdot (T_{ext} - T)$$

With  $h$ , the HT coefficient which depends on:

- The area of the body
- The time
- The cooling fluid nature
- The cooling fluid velocity
- The cooling fluid temperature
- The convection conditions

With  $T_{ext}$ , the cooling fluid temperature



# Modelling interface

## Energetic materials

	TB I180	
State	Solid	Liquid
Density		
Specific Heat capacity (J.kg <sup>-1</sup> .K <sup>-1</sup> )	Censored	Censored
Thermal Conductivity (W.m <sup>-1</sup> .K <sup>-1</sup> )		
Thermal diffusivity (mm <sup>2</sup> .s <sup>-1</sup> )	Censored	Censored
Solidification point (°C)		
Heat of solidification (kJ.kg <sup>-1</sup> )		



TB I180

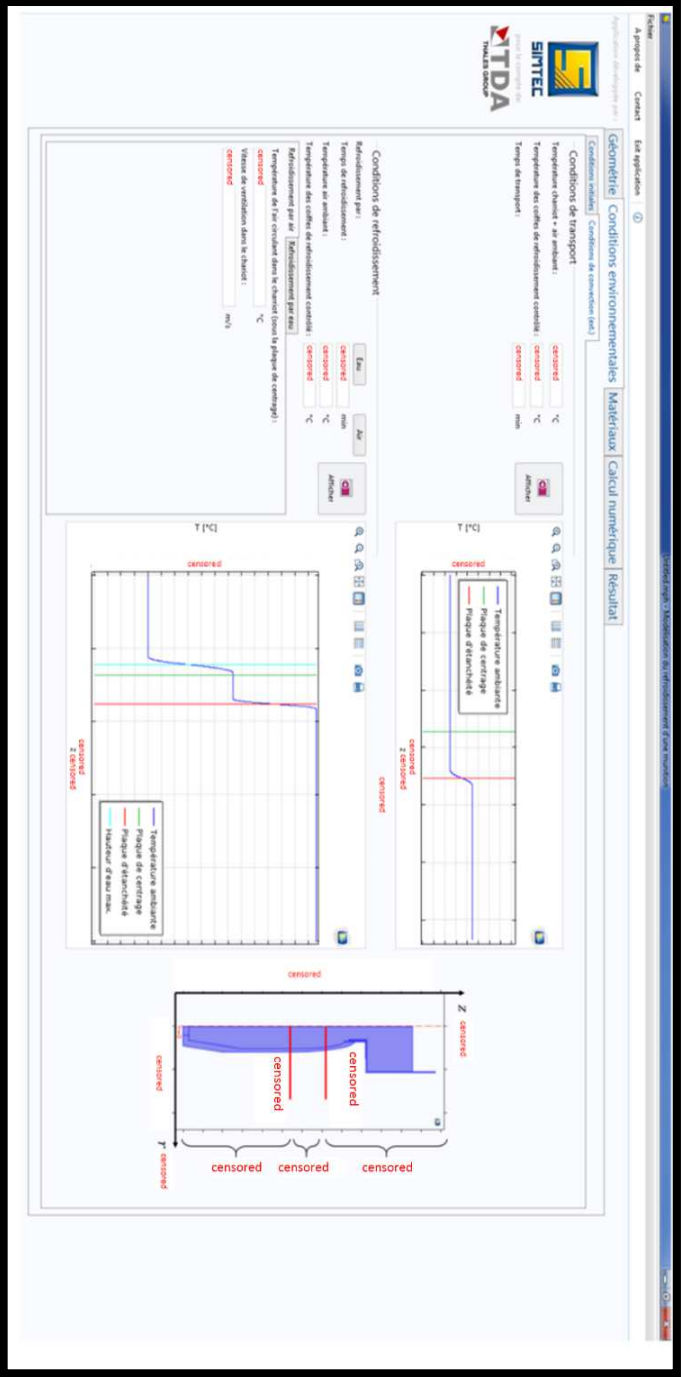




# Modelling interface

## Implementation on customized interface

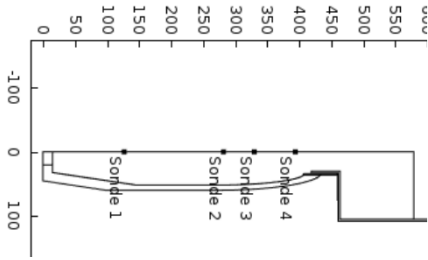
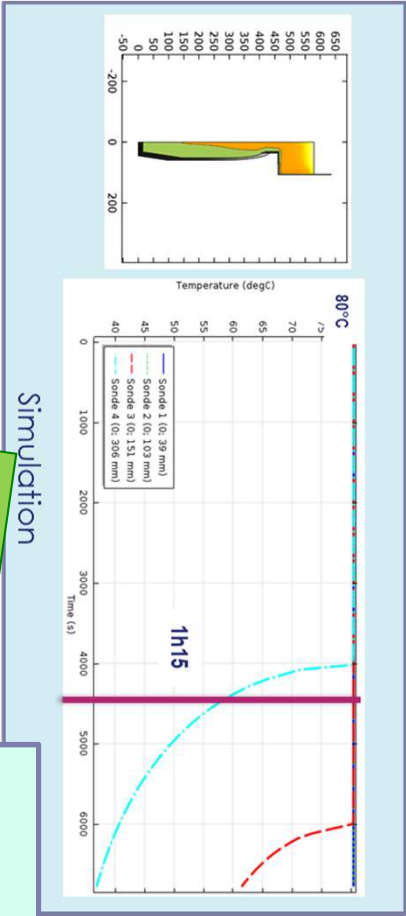
➤ Using COMSOL Multiphysics software



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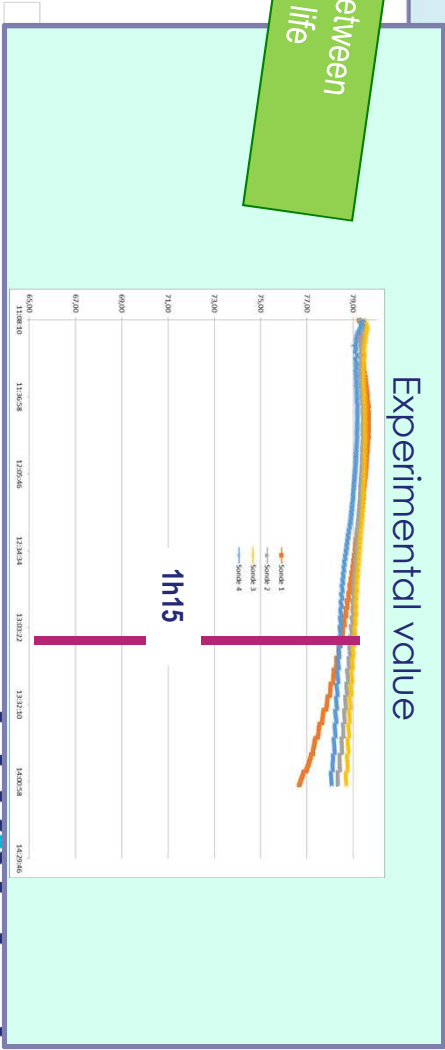
# Modelling interface

## Correlation and validation



Probe positions

Good correlation between  
simulation and real life



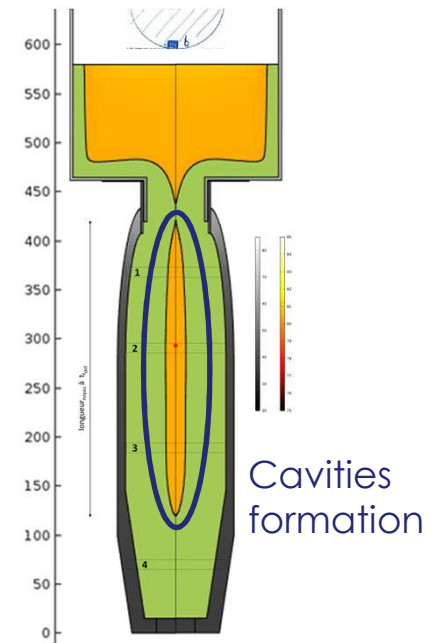
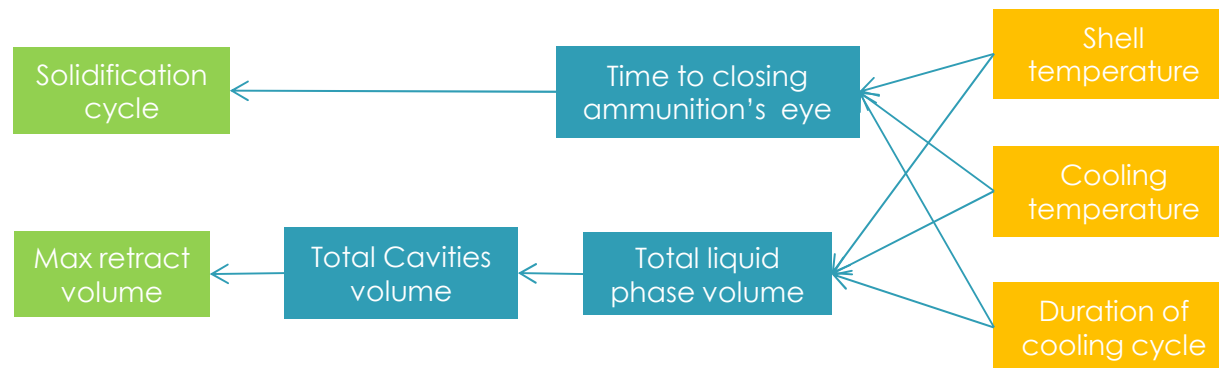
1h15

1h15

# Theoretical study on retract

## Phenomena analyses

- Retracts are linked to different liquid and solid densities

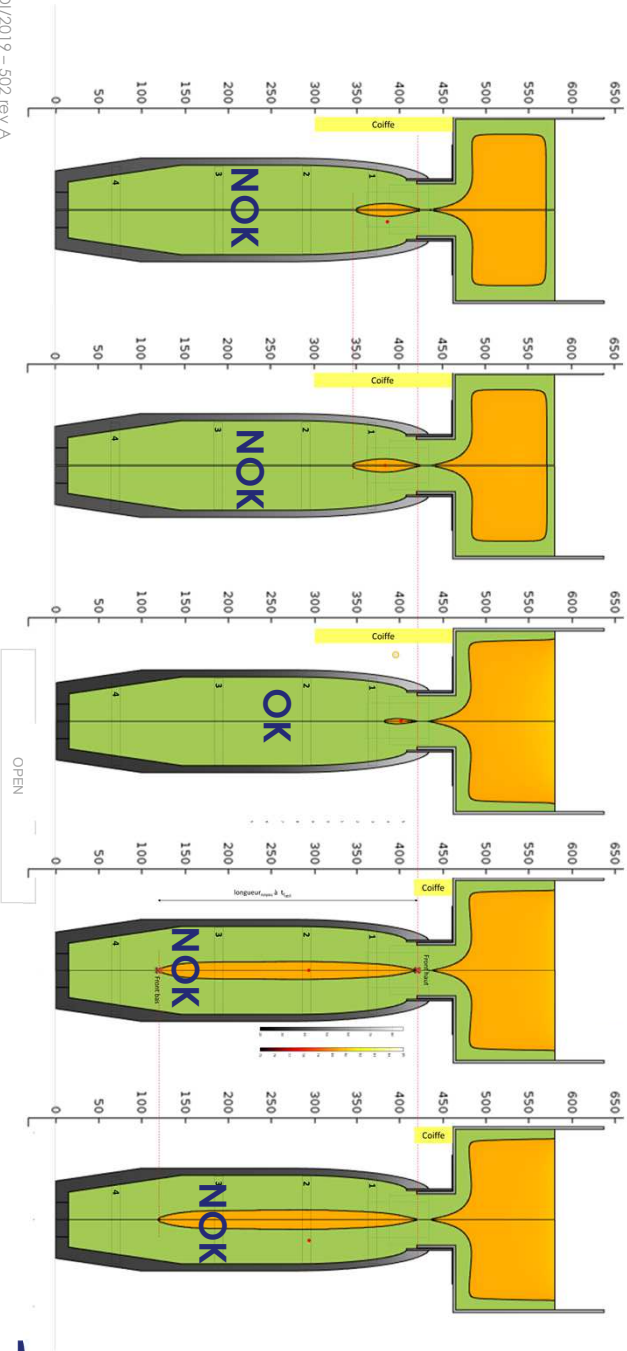


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# Theoretical study on retract

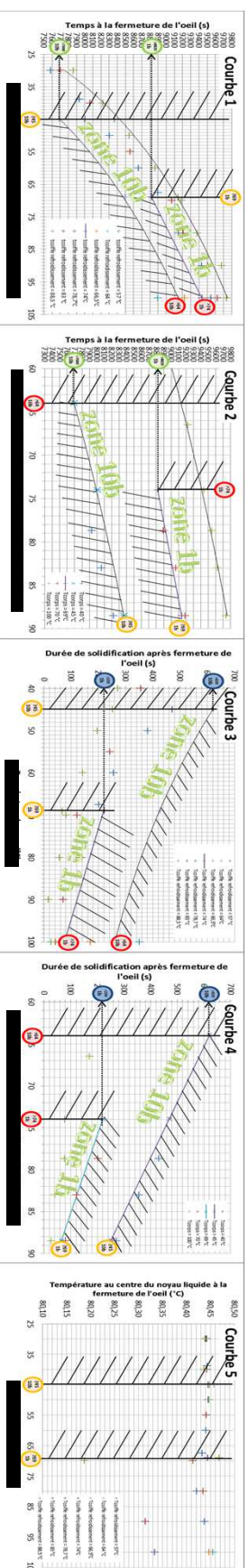
## Some Results

- Shell temperature : 83 °C
- Colling temperature : 50 °C



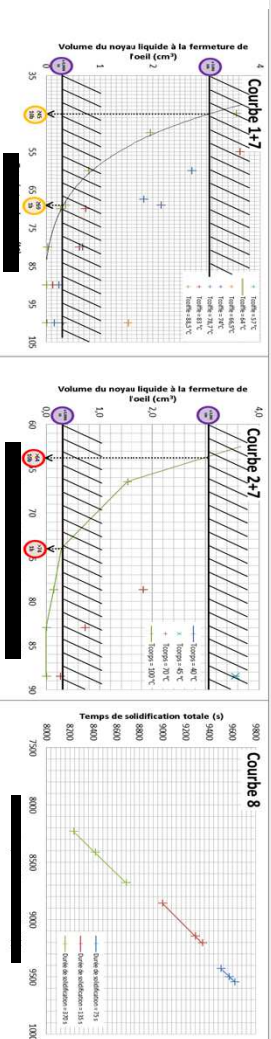
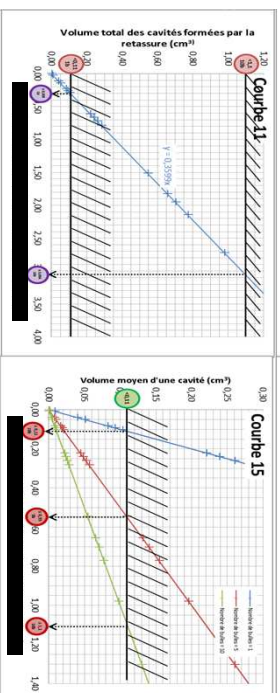
# Theoretical study on retract

## Determination of industrial parameters



Two working zones:

Shell temperature > 69 °C  
And  
Cooling temperature > 74 °C



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# Conclusion



## Development of HMI modelling solidification of melt-cast process

- Requires lots of industrial data
- Needs of design parameters
- Characterization of formulations

## Useful for

- Mastering the production process
- Implementation of new ammunition design or formulation to industrial scale

## Future

- Optimization for implementation of retract

## Log of changes and approval

### Log of changes

Revisions	Description	Date
001	Creation	
002		
003		

### Approval

Actors	Name and role	Signature	Date
Written by	T. GILLOUX		
Verified by	C. COULOUARN		
Approved by	P. DOIGNON		